

SuDSmart



Sustainable Drainage Assessment

Site Address

New Zealand House 160 Abbey Foregate Shrewsbury SY2 6FD

Grid Reference

520291, 260888

Report Prepared for

Mr John Smith Design House Architect Road Plan City SY63 87X

Date

September 2020

Report Status FINAL Site Area

0.3 ha

Report Reference SuDSmart Example



Infiltrate to Ground

Discharging via infiltration requires 14.1m^3 of attenuation to be provided to ensure there is no flooding as a result of the development in all storm events up to and including the 1 in 100 year (6 hour storm) including a 40% allowance for climate change. This volume is subject to the results of infiltration testing and would ensure runoff is not increased above the greenfield scenario.

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1 Executive summary



This report assesses the feasibility of a range of Sustainable Drainage Scheme (SuDS) options in support of the Site development process. A SuDS strategy is proposed to ensure surface water runoff can be managed effectively over the lifetime of the development.

SuDS suitability

| Risk | lssue | Result |
|-----------|---|--------------------|
| | What is the infiltration potential at the Site? | Moderate to High |
| Discharge | What is the potential to discharge to surface water features? | High |
| Location | What is the potential to discharge to sewers? | Low |
| | What is the potential to discharge to highway drains? | Low |
| | What is the fluvial flood risk at the Site? | Very Low to Medium |
| Flooding | What is the pluvial flood risk at the Site? | Very Low |
| | What is the groundwater flood risk at the Site? | Low to Moderate |
| | Is the groundwater a protected resource? | No |
| Pollution | Is the surface water feature a protected resource? | No |

Summary of existing and proposed development

The Site is currently used within a commercial capacity. At present there is a single building with car park and landscaped areas. Development proposals comprise the construction of a new commercial building while keeping the existing features already located on the Site along with the installation of permeable paving.

Summary of discharge routes

GeoSmart's SuDS Infiltration Potential (SD50) map indicates the Site has a moderate to high potential for infiltration, primarily due to the high permeability of the underlying geology (river terrace deposits and sandstone). Infiltration to ground is therefore likely to be feasible.

Ordnance Survey (OS) mapping indicates a surface water feature is located within 60 m south of the Site. Therefore, discharge into this feature should be considered.

The regulated drainage and water search included in Appendix C confirms the Site is located within 20 m of the public sewer network and currently discharges to this. However due to the



topographic gradient discharging to sewer from the proposed development is not considered to be feasible.

According to Google Streetview, highway gullies are located within Abbey Foregate, indicating the presence of the highway drainage network.

Runoff rate and attenuation requirements

Discharging via infiltration requires 14.1m³ of attenuation to be provided to ensure there is no flooding as a result of the development in all storm events up to and including the 1 in 100 year (6 hour storm) including a 40% allowance for climate change. This volume is subject to the results of infiltration testing and would ensure runoff is not increased above the greenfield scenario.

Discharging off-Site would require 5.5m³ of attenuation to be provided to ensure there is no flooding within the development in all storm events up to and including the 1 in 100 year including a 40% allowance for climate change. This volume is subject to the discharge rate being restricted to 2 l/s.

Recommendations / Next steps

A site investigation is required to confirm the infiltration capacity of the ground in line with BRE 365 guidelines to confirm the infiltration rate and the groundwater level.

A Sustainable Drainage Scheme (SuDS) Strategy should be prepared once development designs are confirmed.

Where site investigation confirms the underlying ground conditions are not conducive to infiltration, the condition and capacity of the surface watercourse should be confirmed and permission to discharge should be obtained from the Environment Agency.





Site location

Figure 1. Aerial Imagery (Bluesky, 2020)







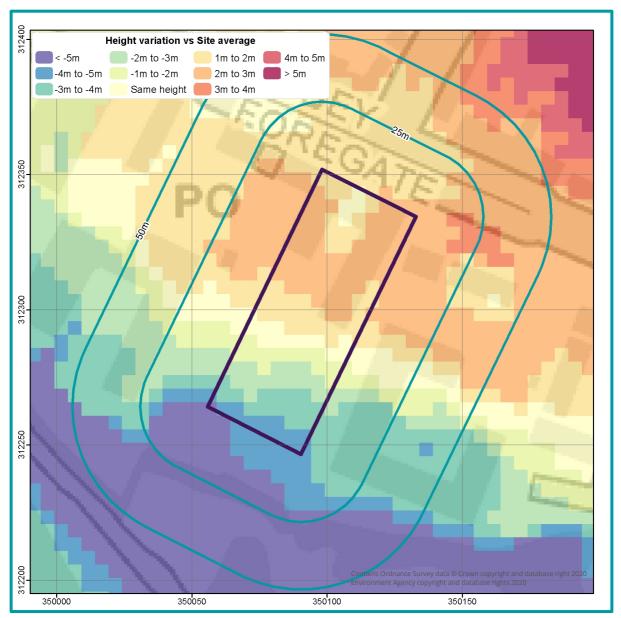
Figure 2. SuDS infiltration suitability (SD50) map (GeoSmart, 2020)

GeoSmart's SuDS Infiltration Suitability (SD50) Map screens the potential for infiltration drainage at the Site and indicates where further assessment is recommended. The map combines information on the thickness and permeability of the underlying material and the depth to the high groundwater table.

According to the SD50 map, there is a moderate to high potential for infiltration SuDS within the Site.

A Site investigation is recommended to investigate groundwater levels and formation thickness and to confirm that infiltration rates at the Site are sufficient to accommodate an infiltration SuDS feature.







GeoSmart have undertaken an assessment of the topography at the Site and within its vicinity, using LiDAR elevation data from the Environment Agency (EA). The mapping shows a comparison between average ground levels on the Site with ground levels in the surrounding area.

The topographic data confirms the general level of the Site falls in a south westerly direction from 57.2 mAOD along the north eastern boundary to 51.6 mAOD along the south western boundary.

The EA LiDAR elevation obtained for the Site was to a 1m resolution with a vertical accuracy of ± 150 mm.



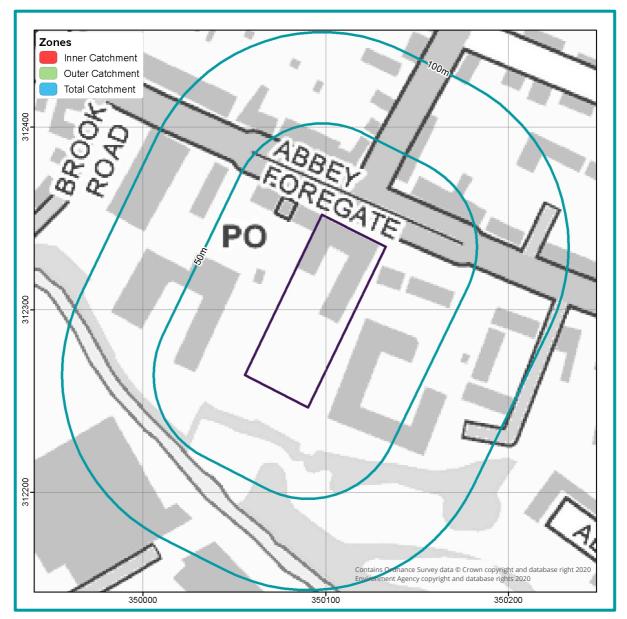


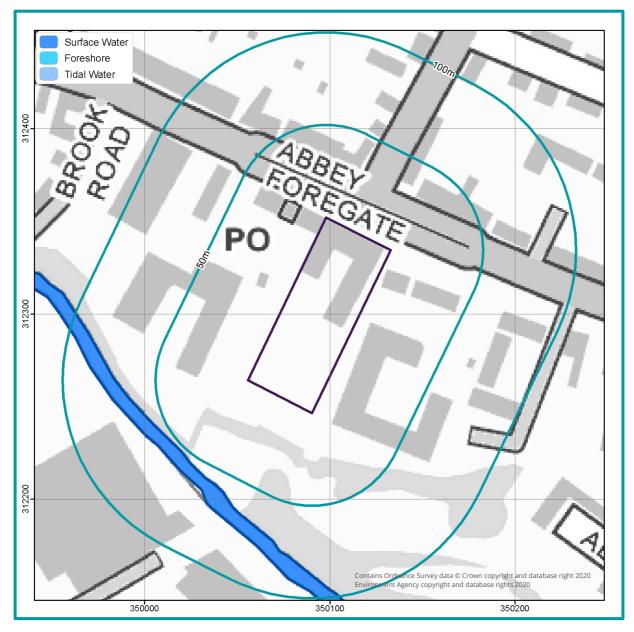
Figure 4. Source protection zone map (EA, 2020)

GeoSmart have undertaken an assessment of the EA groundwater Source Protection Zones (SPZ) within the vicinity of the Site.

The Site is not within a SPZ, therefore, if applicable, infiltration to the ground is likely to be acceptable providing suitable mitigation measures are in place if required to prevent an impact on water quality from the proposed or historical land use.

If hazards are identified, further consideration of the potential for any drainage system to cause pollution of groundwater is recommended. It is also recommended that the Local Authority and the EA are contacted to confirm the susceptibility of controlled water within the wider area.





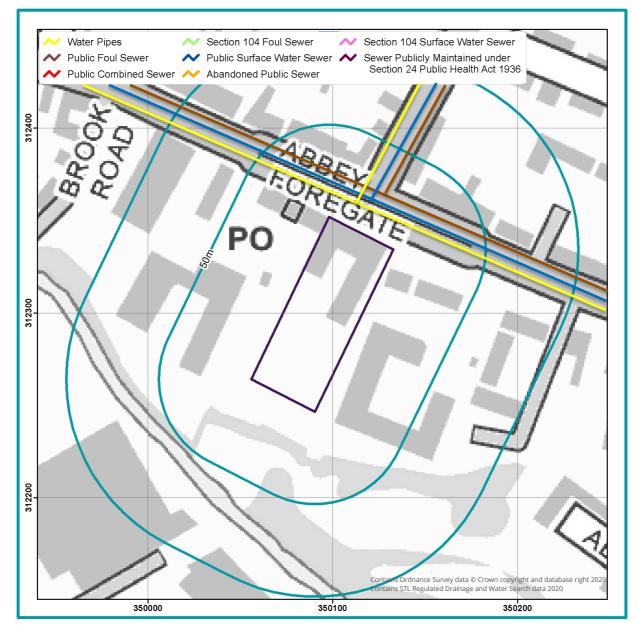


GeoSmart have undertaken an assessment of the location of surface water features within the vicinity of the Site. The Rea Brook is located 55m south west of the Site and discharge to this watercourse is likely to be feasible.

Further analysis could be undertaken by visiting the Site or by contacting the Local Council and the EA to confirm the presence, location and condition of these watercourses.







GeoSmart have undertaken an assessment of the location of sewer features within the vicinity of the Site. A public surface water sewer is located within Abbey Foregate. Discharge to sewer is unlikely to be feasible however as the topography of the Site falls steeply away from the sewer.

Further analysis of the connections and condition of the public surface water and foul drainage systems should be undertaken by carrying out a CCTV survey, or by contacting the drainage provider or the Local Council to confirm the presence, location and condition of these sewers. Consultation with the drainage provider would also be required to determine that sufficient capacity is available to accept the proposed discharge, and to gain permission to connect if required.



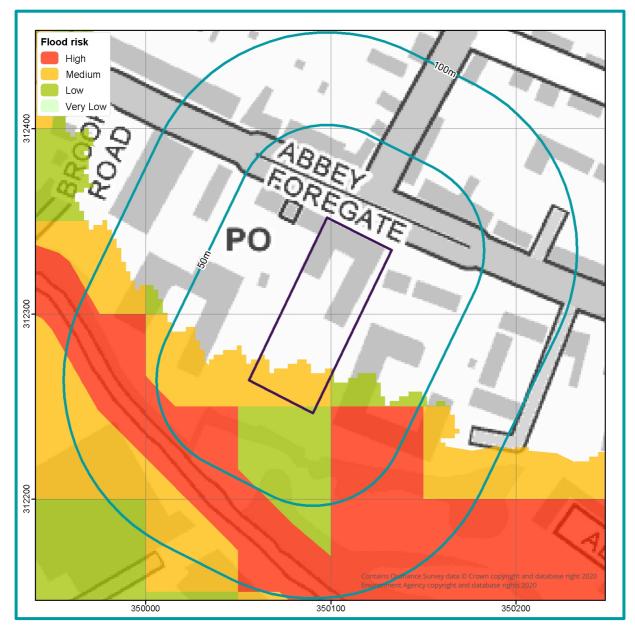


Figure 7. Risk of flooding from rivers & sea map (EA, 2020)

GeoSmart have undertaken an assessment of the risk of flooding from the rivers and the sea within the vicinity of the Site.

The majority of the Site is located at a negligible risk of flooding however the south of the Site is at medium risk of flooding.

Where there is a medium or high risk, further analysis could be undertaken by visiting the Site or by contacting the Local council and the EA to confirm the risk and the associated flood depths.



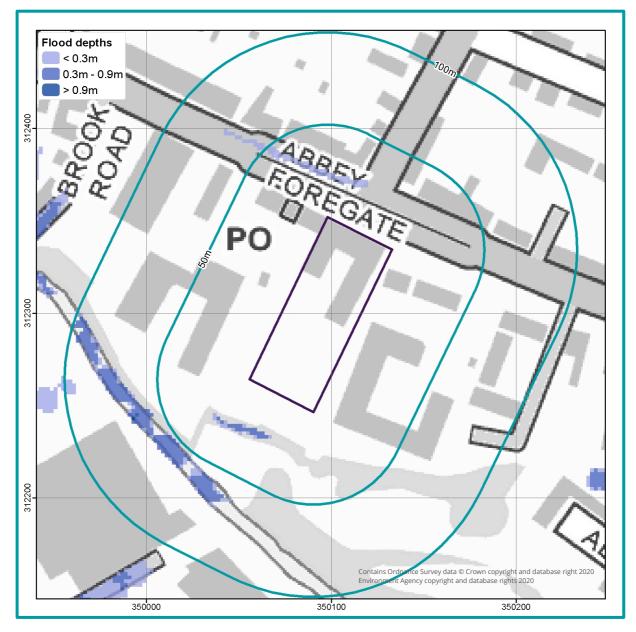


Figure 8. Risk of surface water flooding map (EA,2020)

GeoSmart have undertaken an assessment of the risk of flooding from pluvial sources within the vicinity of the Site. The Site has a very low risk of surface water flooding.

Further analysis could be undertaken by visiting the Site or by contacting the Local Council and the EA; to confirm the pluvial flood risk and flood depths and velocities where applicable.



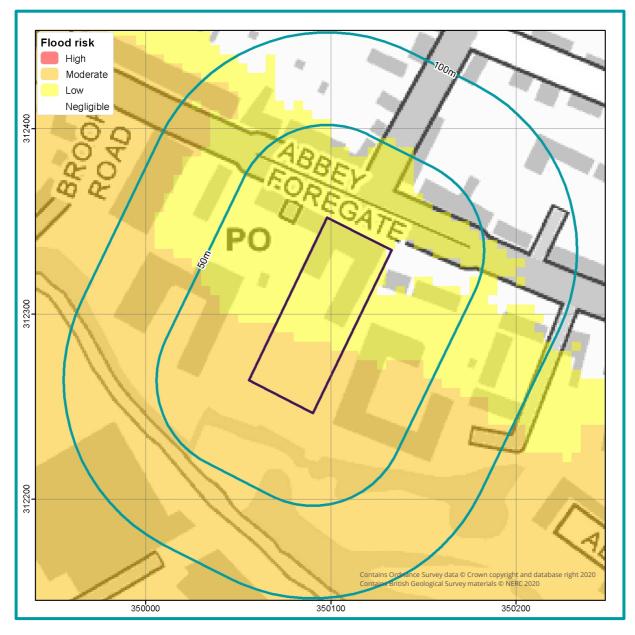


Figure 9. Groundwater flood risk (GW5) map (GeoSmart, 2020)

GeoSmart have undertaken an assessment of the risk of flooding from groundwater sources within the vicinity of the Site. The Site has a low to moderate risk of groundwater flooding.

Therefore, SuDS design could potentially be affected by flooding through the underlying geology. It is necessary that any SuDS are designed to operate in times when groundwater levels are high, so Site specific investigation is necessary to establish the depth to groundwater.



3 Site context

Site information

The purpose of this report is to assess the potential for disposing of surface water through a sustainable drainage system (SuDS) for the site of New Zealand House, 160 Abbey Foregate, Shrewsbury, SY2 6FD (the Site). The Site is located at the centre of Shrewsbury in a setting of commercial and residential use. Site plans and drawings are provided in Appendix A.

Development

The Site is currently used within a commercial capacity. At present there is a single building with car park and landscaped areas. Development proposals comprise the construction of a new commercial building while keeping the existing features already located on the Site.

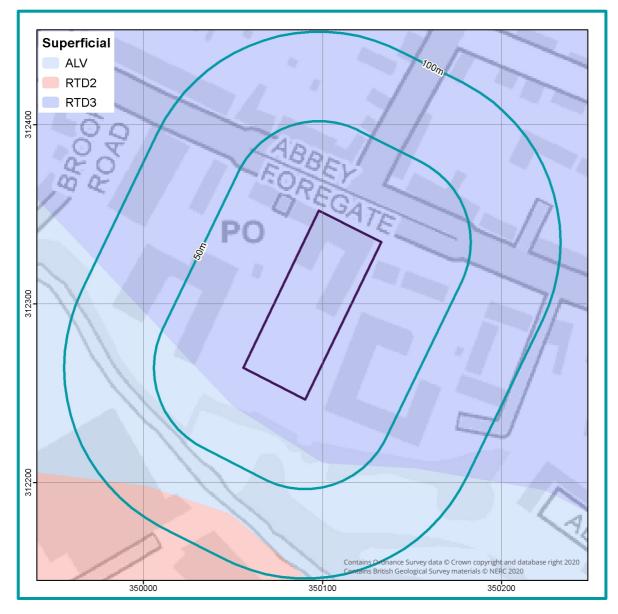
Geology, permeability and thickness

British Geological Survey (BGS) national superficial and bedrock geology mapping confirms a number of different formations underlie the site and each formation may have a range of permeability.

Table 1.Site Geology

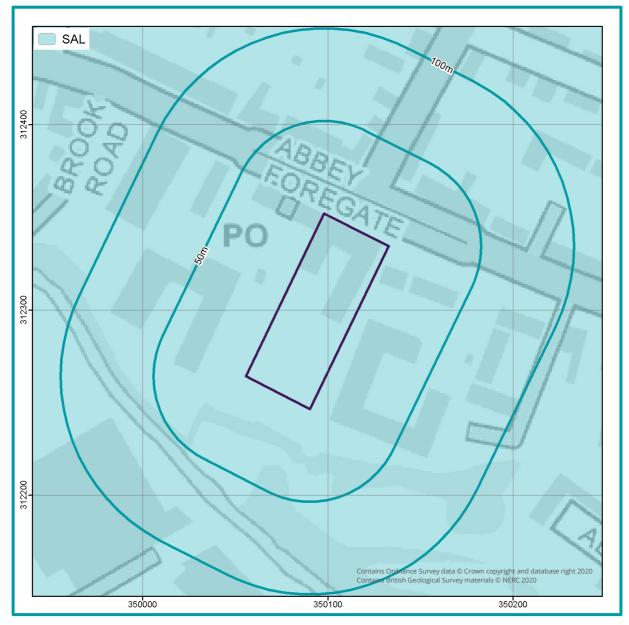
| G | Potentially permeable? | |
|---------------------|-----------------------------------|---|
| Superficial geology | River terrace deposits (RTD3) | ~ |
| Bedrock geology | Salop formation (sandstone) (SAL) | ✓ |













Surrounding borehole records (ref: SJ51SW11) were obtained from the BGS website, these are located approximately 300m to the east of the Site.

The borehole records confirm the underlying geology in the surrounding area comprises of gravelly topsoil to a depth of 0.3m below ground level (bgl) underlain by firm brown clayey silt to a depth of 6.25m bgl where the borehole ends.

The permeability of the underlying material at the Site is likely to be relatively high and confirmation of the infiltration capacity is recommended.

The soil infiltration coefficient must be sufficient to accommodate the constraints on the dimensions of the soakaway and its emptying time.

Infiltration SuDs are proposed directly into permeable superficial deposits.



Depth to groundwater

According to GeoSmart's Groundwater Flood Risk (GW5) map, shallow groundwater is potentially a problem at the Site.

The base of the infiltration system needs to be 1 m above the expected seasonal high-water table. Passage through unsaturated soil is important for improving the quality of infiltrating water before it reaches the water table.

The SuDS system should be designed to operate in periods of extreme groundwater levels.

Guidance

'It is essential that the consideration of sustainable drainage takes place at the land acquisition due diligence stage'

LASOO (2015), Practice Guidance, Local Authority SuDS Officer Organisation.

Ground conditions

A Site specific review of underlying ground conditions is recommended to ensure focused infiltration does not cause ground instability as a result of landslide or collapse associated with dissolution or shallow mining. Hazards that should be considered include soluble rocks, landslides, compressible ground, collapsible ground, shrink-swell clays, running sand and shallow mining.

Soakaways should be a minimum of 5m away from the foundations of a building and local guidance may recommend a greater distance, such as 10m on some areas of Chalk. A detailed ground assessment is recommended: on steep slopes where infiltrating water would produce saturation and instability downslope; or within layered geology, where infiltrating water would produce springs down gradient.



4 Water quality

The Site does not lie within an SPZ. The infiltrated water quality should be of sufficient quality that it does not give rise to pollution of the underlying groundwater. Further consultation with the water company is unlikely to be required.

Infiltration systems should not be used where there is a risk of contaminating groundwater by infiltrating polluted runoff or where receiving groundwater is particularly sensitive.

The influence of surface runoff on water quality will depend on whether there is a source of contamination on Site and the sensitivity of the receiving environment, either groundwater or surface water. The intervening pathway from source to receptor including mitigation and natural attenuation will determine the final impact.

The impact of contaminants on the groundwater will be reduced by travel and natural attenuation through the unsaturated soil zone. A greater depth of unsaturated zone and the presence of significant clay and organic material will provide greater protection for the underlying groundwater. Rapid flow through fractures will provide less protection than intergranular flow around soil and rock particles.



5 National & local policy context



CIRIA SuDS Manual (C753) (2015)

A development should utilise sustainable drainage systems (SUDS) unless there are practical reasons for not doing so, and should aim to achieve greenfield run-off rates and ensure that surface water run-off is managed as close to its source as possible in line with the following drainage hierarchy:

- 1. Use infiltration techniques, such as porous surfaces in non-clay areas,
- 2. attenuate rainwater in ponds or open water features for gradual release,
- 3. attenuate rainwater by storing in tanks or sealed water features for gradual release,
- 4. discharge rainwater direct to a watercourse,
- 5. discharge rainwater to a surface water sewer / drain,
- 6. discharge rainwater to the combined sewer.

Defra - Sustainable Drainage Systems: Non-statutory technical standards for sustainable drainage systems (2015)

Peak Flow control

For developments which were previously developed, the peak runoff rate from the development to any drain, sewer or surface water body for the 1 in 1 year rainfall event and the 1 in 100 year rainfall event must be as close as reasonably practicable to the greenfield runoff rate from the development for the same rainfall event, but should never exceed the rate of discharge from the development prior to redevelopment for that event.

For greenfield developments, the peak runoff rate from the development to any highway drain, sewer or surface water body for the 1 in 1 year rainfall event and the 1 in 100 year rainfall event should never exceed the peak greenfield runoff rate for the same event.

Volume control

Where reasonably practicable, for developments which have been previously developed, the runoff volume from the development to any highway drain, sewer or surface water body in the 1 in 100 year, 6 hour rainfall event must be constrained to a value as close as is reasonably practicable to the greenfield runoff volume for the same event, but should never exceed the runoff volume from the development site prior to redevelopment for that event. The runoff volume must be discharged at a rate that does not adversely affect flood risk.

The drainage system must be designed so that, unless an area is designated to hold and/or convey water as part of the design, flooding does not occur on any part of the site for a 1 in 30 year rainfall event.

Ministry of Housing, Communities & Local Government – National Planning Practice Guidance: Flood risk assessments: climate change allowances (2014)

The Peak rainfall intensity allowances section provides advice on the increased rainfall effects on river levels and land and urban drainage systems. The anticipated changes in peak rainfall intensity in small catchments (less than 5 km²) and urban catchments are shown in Table 4.

For large rural catchments use the alternative allowances defined for rivers.

In order to understand the range of impact, both the central and upper end allowances should be assessed.

Table 2.Peak rainfall intensity allowance in small and urban catchments (use
1961 to 1990 baseline)

| Applies across all of England | Total potential change anticipated for 2010 to 2039 | Total potential change anticipated for 2040 to 2059 | Total potential change anticipated for 2060 to 2115 |
|----------------------------------|---|---|---|
| Upper end | 10% | 20% | 40% |
| Central | 5% | 10% | 20% |

The drainage system should be designed to make sure there is no increase in the rate of runoff discharged from the site for the upper end allowance.

Where on-site flooding for the upper end allowance presents a significant flood hazard (for example, depths and velocities of surface water runoff cause a significant danger to people), you will need to take further mitigation measures to protect people and property (for example, raising finished floor levels). As a minimum, there should be no significant flood hazard to people from on-site flooding for the central allowance.

Local Policy

Shropshire Council - Surface Water Management: Interim Guidance for Developers

SuDS should, wherever possible, be constructed outside of Flood Zones 2 and 3 as indicated on the Environment Agency's Flood Maps.

As a minimum, developments on greenfield sites should limit surface water runoff to existing greenfield runoff rates for all events up to and including the 1% (100 year return period) design event with an allowance for climate change (20% allowance for nonresidential developments and 30% allowance for residential developments). In proposing the use of SuDS for greenfield development sites the ultimate aim should be for mimicry of the predeveloped site's drainage characteristics or, where necessary, to provide a betterment



(especially where there are flood risk issues experienced downstream of the site). A greenfield site is one that has not previously been developed in any way.

To reduce flood risk downstream, the use of SuDS on brownfield redevelopment sites should reduce the existing rate of surface water runoff by a minimum of 50%. A brownfield site is one that has previously been developed.



6 Storage, volume and peak flow rate



Suggested minimum and aspirational storage requirements for an infiltration or attenuation SuDS scheme for the development footprint are set out below, with more detail provided in subsequent sections. Storage volumes may be reduced (but not below the minimum level) if the design incorporates off-site discharge.

Table 3.Storage requirements at the proposed development Site (Discharge
runoff via infiltration)

| Attenuation scenario | | Attenuation required (m ³) | Explanation | |
|-----------------------------------|---|--|--|--|
| Discharge runoff via infiltration | 1 in 30 year | 7.4 | Attenuation required to ensure surface water runoff is attenuated in all storm events up to and including the 1 in 30 year event*. Flooding of the Site of 2.4 m ³ should be contained within permeable landscaped areas within the Site to ensure no flooding of internal areas during the 1 in 100 year storm event. | should be managed within overland flow routes to ensure there is no increase in flood risk in all events up to the 1 in |
| ischarge runof | 1 in 100 year | 9.8 | Attenuation required to ensure surface water runoff is attenuated in all storm events up to and including the 1 in 100 year event*. | |
| | 1 in 100 year including 40% CC | 14.1 | Attenuation required to ensure surface attenuated in all storm events up to and inclu year event including a 40% allowance for clim | ding the 1 in 100 |

*Subject to confirmation through infiltration testing.



Table 4.Storage requirements at the proposed development Site (Discharge
runoff to surface watercourse)

| Attenuation scenario | | Attenuation required (m ³) | Explanation | |
|---|------------------|--|--|--|
| Discharge runoff to surface watercourse | 1 in 30 year | 1.7 | Attenuation required to ensure surface water runoff is attenuated in all storm events up to and including the 1 in 30 year (0.25 hour, Critical Storm Duration) event*. Flooding of the Site of 1.5 m ³ should be contained within permeable landscaped areas within the Site to ensure no flooding of internal areas during the 1 in 100 year storm event. | should be managed within overland flow routes to ensure there is no increase in flood risk in all events up to the 1 in |
| charge runoff to s | 1 in 100 year | 3.2 | Attenuation required to ensure surface water runoff is attenuated in all storm events up to and including the 1 in 100 year (0.25 hour, Critical Storm Duration) event*. | allowance for |
| NoAttenuation required to ensure surface water attenuated in all storm events up to and including year (0.5 hour, Critical Storm Duration) event inclu- allowance for climate change*. | | ding the 1 in 100 | | |

*See Appendix B for associated runoff and discharge calculations. Discharge rates all restricted to greenfield rates in their respective events.



Surface water runoff

An increase in impermeable area on site will result in greater rainfall runoff. Reduction in runoff will help mitigate flood risk both on and off site. Further information on the surface water runoff calculations is provided in Section 11 'Background Information'.

Guidance

The Non-Statutory Technical Guidance for SuDS (Defra, March 2015) states:

"Where reasonably practicable, for Greenfield development, the runoff volume from the development to any highway drain, sewer or surface water body in the 1 in 100 year, 6 hour rainfall event should never exceed the Greenfield runoff volume for the same event. Where reasonably practicable, for developments which have been previously developed, the runoff volume from the development to any highway drain, sewer or surface water body in the 1 in 100 year, 6 hour rainfall event must be constrained to a value as close as is reasonably practicable to the Greenfield runoff volume for the same event, but should never exceed the runoff volume from the development site prior to redevelopment for that event."

Table 5. Change in impermeable area associated with the development

| Total site area | 3775m ² | |
|---|--|--|
| Impermeable area (and as a percentage of the total area of the proposed development footprint of 150 m ²) | | |
| Pre-development | Post-development | |
| 130 m² (87%) | 150 m² (100%) | |
| Impermeable Land use: car park | New impermeable land use: building roof | |
| Permeable Land use: landscaped areas | | |

Guidance

"The drainage system must be designed so that, unless an area is designated to hold and/or convey water as part of the design, flooding does not occur on any part of the site for a 1 in 30 year rainfall event' and 'flooding does not occur during a 1 in 100 year rainfall event in any part of: a building (including a basement); or in any utility plant susceptible to water (e.g. pumping station or electricity substation) within the development"

(Defra, March 2015, non-statutory guidance).



Only the area intended for building development has been considered for the calculations. The existing commercial building is remaining unchanged and is therefore assumed to drain as existing.

Peak discharge rates

The table below presents peak discharge rates for a range of storm events used to assess the impact of the proposed development and select the maximum permitted discharge rate. Further information on the calculation and control of peak discharge rates is provided in Section 11 'Background Information'.

| Rainfall event | Greenfield runoff rates (l/s) | Existing runoff rates ¹ (l/s) | Potential runoff rates without attenuation (l/s) | Potential minus existing (l/s) |
|-------------------------------|-------------------------------------|---|--|---|
| QBAR | 0.00 | N/A | N/A | N/A |
| 6 hour 1 in 1 year | 0.00 | 0.14 | 0.16 | 0.02 |
| 6 hour 1 in 10 year | 0.00 | 0.24 | 0.28 | 0.03 |
| 6 hour 1 in 30 year | 0.00 | 0.33 | 0.38 | 0.05 |
| 6 hour 1 in 100 year | 0.01 | 0.44 | 0.50 | 0.06 |
| 6 hour 1 in 100 year + 20% CC | N/A | N/A | 0.60 | 0.16 |
| 6 hour 1 in 100 year + 40% CC | N/A | N/A | 0.70 | 0.26 |

Table 6. Peak discharge rates associated with the development

¹ Assumes 100% runoff from impermeable surfaces. Assumes Greenfield runoff from permeable surfaces calculated using the IoH124 method.

Relevant local and regional plan policy should be consulted to determine restrictions on runoff from previously developed sites. In some cases, green field rates may be requested. In practice it is difficult to restrict discharge rates at any one control point to less than 2 l/s.

Total discharge volumes

The table below presents discharge volumes for a range of storm events used to assess the impact of the proposed development and calculate the required storage volumes. Further information on the calculation of total discharge volumes is provided in Section 10 'Methodology and Limitations'.

| Rainfall event | Greenfield runoff volume (m ³) | Existing runoff volume ² (m ³) | Potential runoff volume without attenuation (m ³) | Potential minus existing (m ³) |
|-------------------------------|---|--|---|---|
| QBAR | 0.38 | N/A | N/A | N/A |
| 6 hour 1 in 1 year | 0.35 | 3.09 | 3.51 | 0.42 |
| 6 hour 1 in 10 year | 0.62 | 5.28 | 6.00 | 0.72 |
| 6 hour 1 in 30 year | 0.82 | 7.19 | 8.17 | 0.98 |
| 6 hour 1 in 100 year | 1.08 | 9.54 | 10.84 | 1.30 |
| 6 hour 1 in 100 year + 20% CC | N/A | N/A | 13.01 | 3.47 |
| 6 hour 1 in 100 year + 40% CC | N/A | N/A | 15.18 | 5.64 |

Table 7. Total discharge volumes associated with the development

² Assumes 100% runoff from impermeable surfaces. Assumes Greenfield runoff from permeable surfaces calculated using the IoH124 method.

Critical storm duration and volume requirements

Storage volumes for a range of return periods including the 1 in 30 year, 1 in 100 year and 1 in 100 year plus climate change (40%) events have been calculated to assess the impact of the proposed development. The required storage volumes for attenuation features have been calculated for the critical storm durations, limited to a maximum discharge rate of 2 l/s.

| Return Period | Runoff rate restriction (l/s) | Critical Storm Duration (hr) | Attenuation volume required (m ³) |
|---------------------------------------|----------------------------------|---------------------------------|--|
| 1 in 30 year | 2 | 0.25 | 1.7 |
| 1 in 100 year | 2 | 0.25 | 3.2 |
| 1 in 100 year plus 40% climate change | 2 | 0.5 | 5.5 |

Table 8. Critical Storm Duration and Attenuation volume requirements



7 Runoff destination



Options for the destination for the runoff generated on-site have been assessed in line with the prioritisation set out in the Building Regulations Part H document (HM Government, 2010) and Defra's Non-statutory Technical Standards for SuDS (2015). Flow attenuation using infiltration SuDS (discharge to ground) is generally the preferred option. If discharge to ground is not available, runoff discharge to surface water is the other preferred method. Only if these two options are impractical should discharge to the sewer network be considered.

Discharge to ground

As discussed in the Site has high to moderate potential for infiltration, with permeable underlying gravel. Based on the available borehole information (subject to confirmation by site investigation) and groundwater flood risk mapping there is the potential for occasional high groundwater levels at the southern end of the site in response to rises in water level in the adjacent Rea Brook (See SuDS Infiltration Suitability Map (SD50)). There are no issues identified relating to site contamination or the presence of a source protection zone. A site investigation comprising trial pits is recommended to confirm the depth to groundwater and allow infiltration tests to be undertaken to confirm the feasibility of an infiltration SuDS scheme.

Discharge to surface watercourse

The Rea Brook is located within 50m of the site. It sits at a lower elevation then any potential SuDS scheme would be and is also in the direction of the natural flow path of runoff from the site. If site investigation proves onsite infiltration is not possible, then offsite discharge with flow attenuation and storage is an alternative option. There is a possible offsite discharge route to the River Rea across approximately 50m of neighbouring land. Access would need to be arranged and the outfall would be subject to river Level and flood conditions. The site is partly located within a Flood Zone 3 with the risk of flooding originating from Rea Brook. Therefore, it is advisable that discharge to the nearest surface watercourse is carefully considered.

Discharge to sewer

Discharge to sewer is not likely to be the optimum sustainable drainage option for the new development area. It is understood that the existing site drainage is to the sewer and this may continue for parts of the site outside the development footprint. If required consultation with the local sewer undertaker should be undertaken. Discharge to sewer would only be accepted if it can be demonstrated that none of the above options are reasonably practical. Discharge would have to be controlled and onsite attenuation would be required. The topographic gradient on the Site falls relatively steeply to the south away from the existing



drainage network along the main road. It would be difficult to drain the proposed development under gravity to the nearby sewer network.



8 Water quality 🐖

A key requirement of any SuDS system is that it protects the receiving water body from the risk of pollution. This can be effectively managed by an appropriate "train" or sequence of SuDS components that are connected in series. The frequent and short duration rainfall events are those that are most loaded with potential contaminants (silts, fines, heavy metals and various organic and inorganic contaminants). Therefore, the first 5-10 mm of rainfall (first flush) should be adequately treated with SuDS.

The minimum number of treatment stages will depend on the sensitivity of the receiving water body and the potential hazard associated with the proposed development SuDS Manual (CIRIA, 2015). The proposed development is of low (roof water) hazard. The Site does not lie within an SPZ and therefore additional treatment stages are not required.

| Hazard | Source of hazard |
|----------|--|
| Very Low | Residential roof drainage |
| Low | Residential, amenity uses including low usage car parking spaces and roads, other roof drainage. |
| Medium | Commercial, industrial uses including car parking spaces and roads (excluding low usage roads, trunk roads and motorways). |
| High | Areas used for handling and storage of chemicals and fuels, handling of storage and waste (incl. scrap-yards). |

Table 9. Level of hazard

The recommended minimum number treatment stages suggested for the different runoff waters identified for the proposed development is highlighted in the table below.

Table 10. Minimum number of treatment stages for runoff

| | | Sensitivity of the receiving water body | | | |
|--------|------|---|--------|------|--|
| | | Low | Medium | High | |
| | Low | 1 | 1 | 1 | |
| Hazard | Med | 2 | 2 | 2 | |
| | High | 3 | 3 | 3 | |

Permeable paving and a swale would offer sufficient treatment stages (storage/attenuation, filtration through sub-base and filtration through the unsaturated soil zone).



9 Client checklist

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Prior to installation of the site drainage system it is recommended that the client carries out the following checks to confirm the development proposals. Geosmart would be able to support with any updates required to the drainage scheme, please contact us and we would be happy to provide you with a proposal to undertake the work.

Table 11. Potential SuDS limitations

| Conditions in Non-Statutory Technical Standards (Defra, 2015), limitations to infiltration SuDS | Do these conditions arise at the site? |
|--|---|
| Is the surface runoff greater than the rate at which water can infiltrate into the ground? | |
| Is there an unacceptable risk of ground instability? | |
| Is there an unacceptable risk of mobilising contaminants? | |
| Is there an unacceptable risk of pollution to groundwater? | |
| Is there an unacceptable risk of groundwater flooding? | |
| Is the infiltration system going to create a high risk of groundwater leakage to the combined sewer? | |

Table 12. SuDS design considerations

| Confirm that potential flooding on site in excess of the design storm event and exceedance flow routes have been considered. | |
|--|--|
| Review options for the control of discharge rates (e.g. hydrobrake). | |
| Confirm the owners/adopters of the drainage system. Consider management options for multiple owners. | |
| Is there an unacceptable risk of pollution to groundwater? | |
| Review access and way leave requirements. | |
| Review maintenance requirements. | |



Health and safety considerations for SuDS

GeoSmart Pro reports may include outline strategies or designs to support with development plans. Any drawings or advice provided do not comprise any form of detailed design. Implementation of any conceptual scheme options may constitute 'Construction Work' as defined by CDM Regulations (2015).

The CDM Regulations place specific Health and Safety duties on those commissioning, planning and undertaking construction works. If you are uncertain what this means you should seek the advice of your architect, builder or other competent professional.

GeoSmart does not provide health and safety advisory services but we are required to advise you of your general responsibilities under CDM (visit <u>http://geosmartinfo.co.uk/knowledge-hub/cdm-2015/</u> for more information).

Please remember that detailed design work should be undertaken by a competent professional who might be your engineer, architect, builder or another competent party.



10 Methodology and limitations of study

This report assesses the feasibility of infiltration SuDS and alternative drainage strategies in support of the Site development process. From April 6th 2015 SuDS are regulated by Local Planning Authorities and will be required under law for major developments in all cases unless demonstrated to be inappropriate. What is considered appropriate in terms of costs and benefits by the Planning Authority will vary depending on local planning policy, and Site setting. The Lead Local Flood Authority will require information as a statutory consultee on major planning applications with surface water drainage implications. The National Planning Policy Framework requires that new developments in areas at risk of flooding should give priority to the use of SuDS and demonstrate that the proposed development does not increase flood risk downstream to third parties.

How was the suitability of SuDS estimated for the Site?

There are a range of SuDS options available to provide effective surface water management that intercept and store excess runoff. When considering these options, the destination of the runoff should be assessed using the order of preference outlined in the Building Regulations Part H document (HM Government, 2010) and Defra's National Standards for SuDS (2015):

- 1. Discharge to the ground;
- 2. Discharge to a surface water body;
- 3. Discharge to a surface water sewer;
- 4. Discharge to a local highway drain; and
- 5. Discharge to a combined sewer.

Data sets relating to each of the potential discharge options have been analysed to assess the feasibility of each option according to the hierarchy set out above. Hydrogeological characteristics for the Site are assessed in conjunction with the occurrence of SPZ's to assess infiltration suitability. The Site has been screened to determine whether flood risk from groundwater, surface water, fluvial or coastal sources may constrain SuDs. The distance to surface water bodies and sewers has been reviewed gauge whether these provide alternative options.

GeoSmart SuDS Infiltration Suitability Map (SD50)

The GeoSmart SuDS Infiltration Suitability Map (SD50) screens the suitability for infiltration drainage in different parts of the Site and indicates where further assessment is recommended. In producing the SuDS Infiltration Suitability Map (SD50), GeoSmart used data from the British Geological Survey on groundwater levels, geology and permeability to screen



for areas where infiltration SuDS may be suitable. The map classifies areas into 3 categories of High, Medium and Low suitability for infiltration SuDS. This can then be used in conjunction with additional data on Site constraints to give recommendations for SuDS design and further investigation.

The primary constraint on infiltration potential is the minimum permeability of the underlying material and in some cases the range in permeability may be considerable, ranging down to low. The map classifies these areas as moderate infiltration suitability requiring further investigation. In cases where the thickness of the receiving permeable horizon is less than 1.5 meters then additional Site investigation is recommended. If the Site is at risk of groundwater flooding for up to the 1% annual occurrence the map classifies these areas as moderate infiltration suitability requiring further investigation.

The GeoSmart SuDS Infiltration Suitability Map (SD50) is a national screening tool for infiltration SuDS techniques but a Site specific assessment should be used before final detailed design is undertaken. Further information on the GeoSmart SuDS Infiltration Suitability Map (SD50) is available at geosmartinfo.co.uk

How is the suitability to discharge to sewers and watercourses calculated?

The suitability to discharge to discharge to sewers and watercourses has been calculated using the distance from the Site to both. For example, where the Site is within 50m of a surface water body. Discharge to surface water is potentially appropriate subject to land access arrangements and a feasibility assessment. Where the Site is within 50m of a sewer, discharge to sewer is potentially appropriate subject to land access arrangements and a feasibility appropriate subject to land access arrangements and a feasibility appropriate subject to land access arrangements and a feasibility assessment. The utility company should be contacted to agree connection feasibility and sewer capacity.

Further information relating to sewers available in the area can be found in Appendix A.

What is a Source Protection Zone?

The Environment Agency have defined Source Protection Zones (SPZs) for 2000 groundwater sources such as wells, boreholes and springs used for public drinking water supply. These zones show the risk of contamination from any activities that might cause pollution in the area. The closer the activity, the greater the risk. The maps show three main zones (inner, outer and total catchment) and a fourth zone of special interest, which is occasionally applied. The zones are used to set up pollution prevention measures in areas which are at a higher risk. The shape and size of a zone depends on the condition of the ground, how the groundwater is removed, and other environmental factors. Inner zone (Zone 1) is defined as the 50 day travel time from any point below the water table to the source (minimum radius of 50 metres). Outer zone (Zone 2) is defined by a 400 day travel time. Total catchment (Zone 3) is defined as the area around a source within which all groundwater recharge is presumed to be discharged at the source.



How was surface water runoff estimated from the site?

In accordance with The SuDS Manual (C753) (CIRIA, 2015), the Greenfield runoff from the Site has been calculated using the IoH124 method and is assumed representative of the runoff generated on the undeveloped surfaces that are affected by the proposed development. The method used for calculating the runoff complies with the NPPF (DGLC, 2014). For the impermeable surfaces, it has been assumed that 100% runoff will occur (calculations provided in Appendix A). Rainfall data is derived from the Flood Estimation Handbook (FEH) CD-ROM, developed by NERC (2009). Only areas affected by the proposed development are considered in the flow and volume calculations. Permeable areas that remain unchanged are not included in the calculations as it is assumed these will not be actively drained and attenuated.

What is the peak discharge rate?

An estimation of peak runoff flow rate and volume is required to calculate infiltration, storage and discharge requirements. The peak discharge rate is the maximum flow rate at which surface water runoff leaves the site during a particular storm event, without considering the impact of any mitigation such as storage, infiltration or flow control. Proposed discharge rates (with mitigation) should be no greater than existing rates for all corresponding storm events. If all drainage is to infiltration there will be no discharge off site. Discharging all flow from site at the existing 1 in 100 event would increase flood risk during smaller events. Flow restriction is generally required to limit the final discharge from site during all events as a basic minimum to the green field QBAR rate. A more complex flow restriction which varies the final discharge rate from the site depending on the storm event will reduce the volume of storage required on site. Drainage to infiltration SuDS is subtracted from the total discharge off site to achieve a beneficial net affect.

What is the total discharge volume?

The total discharge volume is calculated on the basis of the surface water runoff that has the potential to leave the site as a result of the assumed 6 hour duration design storm event. The runoff is related to the underlying soil conditions, impermeable cover, rainfall intensity and duration of the storm event. The total volume generated by the current site is compared to the potential total volume from the developed site (not taking into consideration any mitigation). The difference provides the minimum total volume that will need to be stored and infiltrated on site or released at a controlled rate. Guidance indicates that the total discharge volume should never exceed the runoff volume from the development site prior to redevelopment for that event and should be as close as is reasonably practicable to the Greenfield runoff volume.



11 Background SuDS information

SuDS control surface water runoff close to where it falls. SuDS are designed to replicate, as closely as possible, the natural drainage from the Site before development to ensure that the flood risk downstream does not increase as a result of the Site being developed, and that the Site will have satisfactory drainage under current and likely future climatic conditions. SuDS provide opportunities to reduce the causes and impacts of flooding; remove pollutants from urban runoff at source; and combine water management with green space with benefits for amenity, recreation and wildlife. Government planning policy and planning decisions now include a presumption in favour of SuDS being used for all development Sites, unless they can be shown to be inappropriate.

For general information on SuDS see our web site: <u>http://geosmartinfo.co.uk/</u>

Infiltration SuDS

Government policy for England is to introduce sustainable drainage systems (SuDS) via conditions in planning approvals. Guidance indicates that capturing rainfall runoff on site and infiltrating it into the ground (infiltration SuDS) is the preferred method for managing surface water without increasing flood risk downstream.

The greatest benefit to general flood risk is if all runoff is infiltrated on site, however, this may not be feasible due to physical and economic constraints in which case infiltration may be considered as a part of an integrated drainage solution. The final design capacity for an infiltration SuDS system depends on the site constraints and the requirements of the individual Planning Authority and the Lead Local Flood Authority.

The capacity of the ground to receive infiltration depends on the nature, thickness and permeability of the underlying material and the depth to the high groundwater table. The final proportion of the site drained by infiltration will depend on topography, outfall levels and a suitable drainage gradient. It is important to note that, even if the whole site cannot be drained by infiltration, the use of partial infiltration is encouraged, with the remainder of runoff discharged via other SuDS systems.

Types of infiltration SuDS

Infiltration components include infiltration trenches, soakaways, swales and infiltration basins without outlets, rain gardens and permeable pavements. These are used to capture surface water runoff and allow it to infiltrate (soak) and filter through to the subsoil layer, before returning it to the water table below.

An infiltration trench is usually filled with permeable granular material and is designed to promote infiltration of surface water to the ground. An infiltration basin is a dry basin or depression designed to promote infiltration of surface water runoff into the ground. Soakaways are the most common type of infiltration device in the UK where drainage is often connected to over-sized square or rectangular, rubble-filled voids sited beneath lawns.



According to the guidance in Building Research Establishment (BRE) Digest 365 (2007) a soakaway must be able to discharge 50% of the runoff generated during a 1 in 10 year storm event within 24 hours in readiness for subsequent storm flow. This is the basic threshold criteria for a soakaway design and the internal surface area of the proposed soakaway design options should be calculated on this basis by taking into account the soil infiltration rate for the Site.

Developers need to ensure their design takes account of the construction, operation and maintenance requirements of both surface and subsurface components, allowing for any machinery access required.

SuDS maintenance and adoption

Regular maintenance is essential to ensure effective operation of the soakaway(s) over the intended lifespan of the proposed development. A maintenance schedule for SuDs is required. Sewerage undertakers or Local Authorities may adopt SuDS and will require maintenance issues to be dealt with in accordance with their Management Plan. If the SuDS will not be adopted other provision is required with associated financial implications. Maintenance is a long-term obligation requiring the upkeep of all elements of the SuDS, including mechanical components (e.g. pumps), as well as inspections, regular maintenance and repair.

Additional background SuDS information can be found on our website: <u>http://geosmartinfo.co.uk/</u>



12 Further information



The following table includes a list of additional products by GeoSmart:

Additional GeoSmart Products

| ✓ | Additional assessment: SuDSmart Report | | The SuDSmart Report range assesses which drainage options are available for a Site. They build on technical detail starting from simple infiltration screening, and work up to more complex SuDS Assessments detailing alternative options. Please contact info@geosmartinfo.co.uk for further information. | |
|---|--|--|--|--|
| ✓ | Additional assessment: FloodSmart Report | | The FloodSmart Report range provides clear and pragmatic advice regarding the nature and potential significance of flood hazards which may be present at a site. Our consultants assess available data to determine the level of risk based on professional judgement and years of experience. Please contact info@geosmartinfo.co.uk for further information. | |
| ~ | Additional assessment: <mark>EnviroSmart Report</mark> | | Provides a robust desk-based assessment of potential contaminated land issues, taking into account the regulatory perspective. Our EnviroSmart reports are designed to be the most cost effective solution for planning conditions. Each report is individually prepared by a highly experienced consultant conversant with Local Authority requirements. Ideal for pre-planning or for addressing planning conditions for small developments. Can also be used for land transactions. Please contact info@geosmartinfo.co.uk for further information. | |



13 References and glossary

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Glossary

General terms

| Attenuation | Reduction of peak flow and increased duration of a flow event. |
|------------------------|---|
| Combined sewer | A sewer designed to carry foul sewage and surface water in the same pipe. |
| Detention basin | A vegetated depression, normally is dry except after storm events, constructed to store water temporarily to attenuate flows. May allow infiltration of water to the ground. |
| Evapotranspiration | The process by which the Earth's surface or soil loses moisture by evaporation of water and by uptake and then transpiration from plants. |
| FEH | Flood Estimation Handbook, produced by Centre for Ecology and Hydrology, Wallingford (formerly the Institute of Hydrology). |
| Filter drain or trench | A linear drain consisting of a trench filled with a permeable material, often with a perforated pipe in the base of the trench to assist drainage, to store and conduct water, but may also be designed to permit infiltration. |
| First flush | The initial runoff from a site or catchment following the start of a rainfall event. As runoff travels over a catchment it will collect or dissolve pollutants, and the "first flush" portion of the flow may be the most contaminated as a result. This is especially the case for intense storms and in small or more uniform catchments. In larger or more complex catchments pollution. |
| Flood plain | Land adjacent to a watercourse that would be subject to repeated flooding under natural conditions (see Environment Agency's Policy and practice for the protection of flood plains for a fuller definition). |
| Greenfield runoff | This is the surface water runoff regime from a site before development, or the existing site conditions for brownfield redevelopment sites. |
| Impermeable surface | An artificial non-porous surface that generates a surface water runoff after rainfall. |
| Permeability | A measure of the ease with which a fluid can flow through a porous medium. It depends on the physical properties of the medium, for example grain size, porosity and pore shape. |
| | |



| Runoff | Water flow over the ground surface to the drainage system. This occurs if the ground is impermeable, is saturated or if rainfall is particularly intense. |
|---------------------|--|
| Sewerage undertaker | This is a collective term relating to the statutory undertaking of water companies that are responsible for sewerage and sewage disposal including surface water from roofs and yards of premises. |
| Soakaway | A subsurface structure into which surface water is conveyed to allow infiltration into the ground. |
| Treatment | Improving the quality of water by physical, chemical and/or biological means. |

The terms included in this glossary have been taken from CIRIA (2015) guidance.

Data Sources

| Aerial Photography | Contains Ordnance Survey data © Crown copyright and database right 2020 BlueSky copyright and database rights 2020 |
|---|--|
| Bedrock & Superficial Geology | Contains British Geological Survey materials © NERC 2020 Ordnance Survey data © Crown copyright and database right 2020 |
| Flood Risk (RoFRS/Pluvial/Surface Water Features/SPZ) | Environment Agency copyright and database rights 2020 Ordnance Survey data © Crown copyright and database right 2020 |
| Flood Risk (Groundwater) and SuDS infiltration suitability (SD50) | GeoSmart, BGS & OS GW5 (v2.3) Map (GeoSmart, 2020) Contains British Geological Survey materials © NERC 2020 Ordnance Survey data © Crown copyright and database right 2020 |
| Sewer Location | Contains Ordnance Survey data © Crown copyright and database right 2020 Contains STL Regulated Drainage and Water Search data 2020 |
| Topographic Data | OS LiDAR/EA Contains Ordnance Survey data © Crown copyright and database right 2020 Environment Agency copyright and database rights 2020 |







Appendix A 🛛 💮

Site plans





Rainfall runoff calculations

| | | | | | Develo | ped site rur | n-off calcula | tion sheet | | | | | | | | |
|--|------------------------|----------------------------|--------------------------------------|--|-------------------------|-------------------------------|-----------------------------------|------------------|------------------|----------------------------|--|------------------------------|----------------------------------|------------------------------------|------------------------|---------------------|
| | 1 in 1 year | | | 1 | . in 30 yea | • | | | | | | 1 in 100 ye | ar | | 1 | |
| roposed impermeable area | | 0.015 | ha | Proposed impermeable area | 1 | 0.015 | ha | | | | Proposed impermeable area | | 0.015 | ha | | |
| C Factor | | 40% | | CC Factor | | 40% | | | | | CC Factor | | 40% | | | |
| otal volume for urfaces during 6 hour event | | 3.52 | l m ³ | Total volume for surfaces during 6 hour event | | 8.17 | m³ | | | | Total volume for surfaces during 6 hour event | | 10.8 | 84 m ³ | | |
| otal volume for 6 hour event inc CC otal volume for 6 hour event exc CC | | 4.91 3.51 | L m ³ L m ³ | Total volume for 6 hour event inc CC Total volume for 6 hour event exc CC | | 11.44 8.17 | | | | | Total volume for 6 hour event inc Total volume for 6 hour event exc | | | 18 m³ 34 m³ | | |
| Duration | Rainfall 1 yr event | Run-off rate 1 yr event | Run-off rate 1 yr +cc event | Duration | Rainfall 30 yr event | Run-off volume 30 yr event | Run-off volume 30 yr +cc event | | | | Dura | Rainfall tion 100 yr even | Run-off volume t 100 yr event | Run-off volume 100 yr +cc event | | |
| hours | mm | m³ | m³ | hours | mm | m³ | m³ | Outflow at 2 l/s | inflow from rain | Diff (storage required) | - | ours mm | m³ | m³ | Outflow ir at 2 l/s | inflow fron rain |
| 0.25 | 7.00 | 1.05 | 1.47 | 0.25 | 23.31 | 3.50 | 4.90 | 1.80 | 3.50 | 1 1 |) | 0.25 32.9 | <mark>7</mark> 4.95 | 6.92 | 1.80 | 6.9 |
| 0.5 | 8.93 | 1.34 | 1.88 | 0.5 | 30.42 | 4.56 | 6.39 | 3.60 | 4.56 | 0.96 | 5 | 0.5 43.3 | <mark>4</mark> 6.50 | 9.10 | 3.60 | 9.1 |
| 0.75 | 10.23 | 1.53 | 2.15 | 0.75 | 34.78 | 5.22 | 7.30 | 5.40 | 5.22 | -0.18 | 3 | 0.75 49.6 | <mark>4</mark> 7.45 | 10.42 | 5.40 | 10.4 |
| 1 | 11.10 | 1.67 | 2.33 | 1 | 37.87 | 5.68 | 7.95 | 7.20 | 5.68 | -1.52 | 2 | 1 54.4 | <mark>1</mark> 8.16 | 11.43 | 7.20 | 11.4 |
| 2 | 15.55 | 2.33 | 3.27 | 2 | 44.78 | 6.72 | 9.40 | 14.40 | 6.72 | -7.68 | | 2 62.3 | <mark>8</mark> 9.36 | 13.10 | 14.40 | 13.1 |
| 3 | 18.37 | 2.76 | 3.86 | 3 | 48.58 | 7.29 | 10.20 | 21.60 | 7.29 | | | 3 66.4 | | 13.96 | 21.60 | 13.9 |
| 4 | 20.43 | 3.06 | 4.29 | 4 | 51.13 | 7.67 | 10.74 | 28.80 | 7.67 | -21.13 | | 4 69.0 | | 14.50 | 28.80 | 14.5 |
| 5 | 22.06 | 3.31 | 4.63 | 5 | 53.00 | 7.95 | 11.13 | 36.00 | | | | 5 70.8 | | 14.88 | 36.00 | 14.8 |
| 6 | 23.40 | 3.51 | 4.91 | 6 | 54.47 | 8.17 | 11.44 | 43.20 | 8.17 | -35.03 | | 6 72.2 | | 15.18 | 43.20 | 15.1 |
| 8 | 25.50 | 3.83 | 5.36 | 8 | 56.74 | 8.51 | 11.92 | 57.60 | | -49.09 | | 8 74.2 | | 15.59 | 57.60 | 15.5 |
| 10 | 27.11 | 4.07 | 5.69 | 10 | 58.47 | 8.77 8.08 | 12.28 | 72.00 86.40 | | -63.23 -77.42 | | 10 75.6 12 76.9 | | 15.89 | 72.00 86.40 | 15.8 16 1 |
| 12 16 | 28.43 30.50 | 4.26 4.58 | 5.97 6.41 | 12 | 59.89 62.17 | 8.98 9.33 | 12.58 13.06 | 115.20 | | | | 12 76.8 16 78.6 | | 16.13 16.52 | 115.20 | 16.1 16.5 |
| 20 | 30.30 | 4.38 | 6.75 | 20 | 64.01 | 9.60 | 13.44 | 113.20 | | | | 20 80.1 | | 16.84 | 113.20 | 16.8 |
| 24 | 33.57 | 5.04 | 7.05 | 24 | 65.62 | 9.84 | 13.78 | 172.80 | | | | 24 81.5 | | 17.12 | 172.80 | 10.0 |
| 28 | 34.77 | 5.22 | 7.30 | 28 | 67.09 | 10.06 | 14.09 | 201.60 | | | | 28 82.8 | | 17.39 | 201.60 | 17.3 |
| 32 | 35.87 | 5.38 | 7.53 | 32 | 68.49 | 10.27 | 14.38 | 230.40 | | | 3 | 32 84.0 | | 17.65 | 230.40 | 17.6 |
| 36 | 36.88 | 5.53 | 7.74 | 36 | 69.82 | 10.47 | 14.66 | 259.20 | | | 3 | 36 85.3 | | 17.92 | 259.20 | 17.9 |
| 40 | 37.84 | 5.68 | 7.95 | 40 | 71.11 | 10.67 | 14.93 | 288.00 | | | | 40 86.5 | | 18.17 | 288.00 | 18.1 |
| 44 | 38.74 | 5.81 | 8.14 | 44 | 72.36 | 10.85 | 15.20 | 316.80 | 10.85 | -305.95 | 5 | 44 87.7 | | 18.43 | 316.80 | 18.4 |
| 48 | 39.61 | 5.94 | 8.32 | 48 | 73.58 | 11.04 | 15.45 | 345.60 | 11.04 | -334.56 | ā | 48 88.9 | 4 13.34 | 18.68 | 345.60 | 18.6 |

| yr Scenario | CC Scenario |
|--------------|---------------|
| iff (storage | Diff (storage |
| required) | required) |
| 3.15 | 5.12 |
| 2.90 | 5.50 |
| 2.05 | 5.02 |
| 0.96 | 4.23 |
| -5.04 | -1.30 |
| -11.63 | -7.64 |
| -18.44 | -14.30 |
| -25.37 | -21.12 |
| -32.36 | -28.02 |
| -46.47 | -42.01 |
| -60.65 | -56.11 |
| -74.88 | -70.27 |
| -103.40 | -98.68 |
| -131.97 | -127.16 |
| -160.57 | -155.68 |
| -189.18 | -184.21 |
| -217.79 | -212.75 |
| -246.40 | -241.28 |
| -275.02 | -269.83 |
| -303.64 | -298.37 |
| -332.26 | -326.92 |
| | |

Greenfield Site Run-Off Calculations usng the IoH124 method

Greenfield peak run-off rate (QBAR):

| Parameters | Input | Units | Comments |
|------------|-------|-------|---------------------------------|
| Area | 50 | ha | mimimum 50ha |
| SAAR | 637 | mm | FEH CD ROM (NERC, 2009) |
| SPR | 0.10 | N/A | Soil run-off coefficient |
| Region | 4 | N/A | Region on Hydrological area map |
| QBAR | | | |

$\mathbf{Q}_{\mathsf{BAR}(\mathsf{rural})} = \mathbf{1.08AREA}^{0.89} \mathbf{SAAR}^{1.17} \mathbf{SPR}^{2.17}$

Where:

| Q _{BAR(rural)} | is the mean annual flood (a return period of 2.3 years) in l/s |
|---------------------------------|--|
| Q _{BAR(rural)} AREA | is the area of the catchment in km ² (minimum of 0.5km ²) |
| SAAR | is the standard average rainfall for the period 1941 to 1970 in mm |
| SPR | is the soil run-off coefficient |
| | |

Q_{BAR(rural)} can be factored by the UK Flood Studies Report regional growth curves to produce peak flood flows for any return period.

| Q _{BAR(rural)} | = | 7.52 | l/s for 50ha site |
|--------------------------------|---|------|-------------------|
| Divided by 50 to scale down | = | 0.15 | l/s/ha |
| Actual Area of the entire Site | = | 0.02 | ha |

Return Periods (Growth curves obtained from DEFRA report)

| | | | | Peak site run-off rate |
|----------------------|---|----------------------|--------|------------------------|
| Return Period | | Growth Factor | l/s/ha | (I/s) |
| 1 | Q _{BAR(rural)} x | 0.85 | 0.13 | 0.002 |
| 2 | Q _{BAR(rural)} x | 0.89 | 0.13 | 0.00 |
| 5 | Q _{BAR(rural)} x | 1.23 | 0.19 | 0.00 |
| 10 | Q _{BAR(rural)} x | 1.49 | 0.22 | 0.00 |
| 25 | $Q_{BAR(rural)} x$ | 1.87 | 0.28 | 0.00 |
| 30 | Q _{BAR(rural)} x | 1.92 | 0.29 | 0.004 |
| 50 | $Q_{BAR(rural)} x$ | 2.2 | 0.33 | 0.00 |
| 100 | Q _{BAR(rural)} x | 2.57 | 0.39 | 0.01 |
| 200 | $Q_{BAR(rural)} x$ | 2.98 | 0.45 | 0.01 |

Greenfield total run-off volume:

= actual area of the entire site x SPR x 6 hour rainfall depth

| Return Period | 6 hour rainfall (mm) from FEH CD-ROM | Area (ha) | SPR | Total run-off (m ³) |
|---------------|--|-----------|------|---------------------------------|
| 2.3 (QBAR) | 25.04 | 0.02 | 0.10 | 0.4 |
| 1 | 23.4 | 0.02 | 0.10 | 0.4 |
| 10 | 41.11 | 0.02 | 0.10 | 0.6 |
| 30 | 54.47 | 0.02 | 0.10 | 0.8 |
| 100 | 72.27 | 0.02 | 0.10 | 1.1 |

| | Sur | nmary | | |
|---|--|---|--|---|
| Entire site area: | 0.015 | ha | | |
| Climate Change Factor | 40% | | | |
| - | Current | Proposed | | |
| Permeable Surface (ha) | 0.002 | 0.000 | | |
| Impermeable Surface (ha) | 0.013 | 0.015 | | |
| | | | | |
| 1 in 1 year | | | | |
| Greenfield run-off volume total: | 0.35 | m ³ | | |
| RUN-OFF During a 1 in 1 year 6 hour event: | Greenfield Site | Current Development | Proposed Development | Proposed Development +C |
| From permeable surfaces (using GF total run-off) (m ³) | 0.35 | 0.05 | 0.00 | 0 |
| From impermeable surfaces (m ³) | | 3.04 | 3.51 | 4 |
| | | | | |
| TOTAL run-off produced from Site (m ³) | 0.35 | 3.09 | 3.51 | 4 |
| | | | | |
| Difference between greenfield site and proposed +cc dev | /elopment (m³): | | | 4 |
| | | | | 130 |
| | | | | |
| Difference between current and proposed +cc developm | ent (m³): | | | 1 |
| · · · · · · · · · · · · · · · · · · · | | | | 5 |
| | | | | |
| Peak Greenfield run-off rate that must not be exceeded i | n the run-off from the | proposed development (l | /s): | C |
| | | | | |
| 1 in 10 year | | 2 | | |
| Greenfield run-off volume total: | 0.62 | | | |
| RUN-OFF During a 1 in 1 year 6 hour event: | Greenfield Site | Current Development | Proposed Development | Proposed Development +C |
| From permeable surfaces (using GF total run-off) (m ³) | 0.62 | 0.08 | 0.00 | (|
| From impermeable surfaces (m ³) | | 5.20 | 6.00 | 8 |
| | | | | |
| TOTAL run-off produced from Site (m ³) | 0.62 | 5.28 | 6.00 | 8 |
| | | | | |
| | | | | |
| | velopment (m ³): | | | 7 |
| Difference between greenfield site and proposed +cc dev | velopment (m ³): | | | 7 |
| | velopment (m ³): | | | |
| Difference between greenfield site and proposed +cc dev | | · | | 126 |
| | | | | 126 |
| Difference between greenfield site and proposed +cc dev | | | | 126 |
| Difference between greenfield site and proposed +cc dev Difference between current and proposed +cc developm | ent (m³): | proposed development (l | /s): | 126 3 5 |
| Difference between greenfield site and proposed +cc dev | ent (m³): | proposed development (l | /s): | 126 3 5 |
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Regulated Drainage and Water Search



SAMPLE DRAINAGE SEARCH

Email: SAMPLE DRAINAGE SEARCH

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Regulated Drainage & Water Search

Property:

160AbbeyForegate, Shrewsbury

Sewerage Water Company: Severn Trent Water Plc

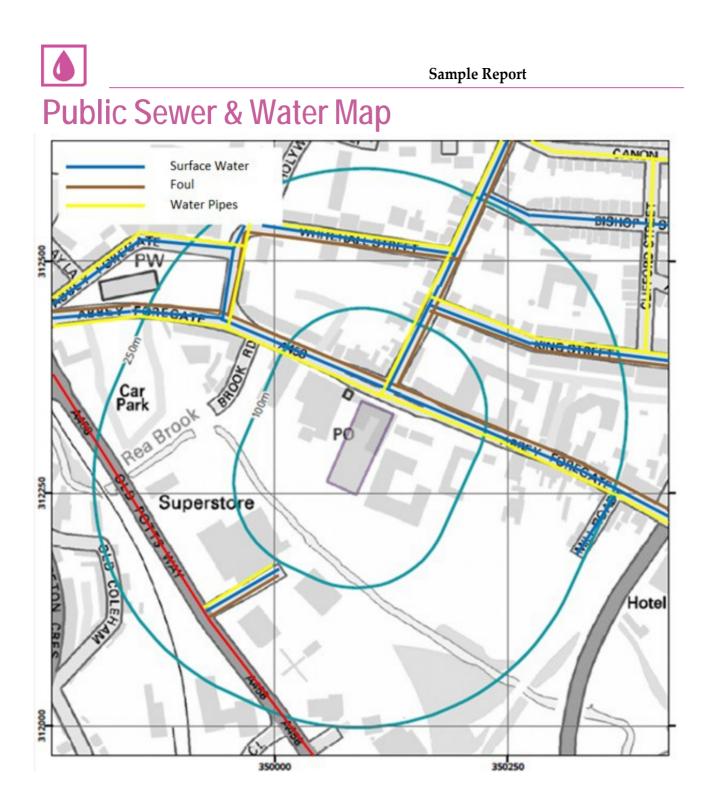
Clean Water Company: Severn Trent Water Plc

Date of Search: 18/05/2016

Reference: 1665925 Client Reference: SAMPLE



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Information on confidence levels and ways to improve this report can be provided for any location on written request to info@geosmart.co.uk or via our website. Updates to our model are ongoing and additional information is being collated from several sources to improve the database and allow increased confidence in the findings. Further information on groundwater levels and flooding are being incorporated in the model to enable improved accuracy to be achieved in future versions of the map. Please contact us if you would like to join our User Group and help with feedback on infiltration SuDS and mapping suggestion.



Important consumer protection information

This search has been produced by GeoSmart Information Limited, Suite 9-11, 1st Floor, Old Bank Buildings, Bellstone, Shrewsbury, SY1 1HU.

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- sets out minimum standards which firms compiling and selling search reports have to meet.
- promotes the best practice and quality standards within the industry for the benefit of consumers and property professionals.
- enables consumers and property professionals to have confidence in firms which subscribe to the code, their products and services.
- By giving you this information, the search firm is confirming that they keep to the principles of the Code. This provides important protection for you.

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Please note that all queries or complaints regarding your search should be directed to your search provider in the first instance, not to TPOs or to the PCCB.

TPOs contact details:

The Property Ombudsman scheme Milford House 43-55 Milford Street Salisbury Wiltshire SP1 2BP Tel: 01722 333306 Fax: 01722 332296 Email: admin@tpos.co.uk

You can get more information about the PCCB from <u>www.propertycodes.org.uk</u>.

Please ask your search provider if you would like a copy of the search code

Complaints procedure

GeoSmart Information Limited is registered with the Property Codes Compliance Board as a subscriber to the Search Code. A key commitment under the Code is that firms will handle any complaints both speedily and fairly. If you want to make a complaint, we will:

- Acknowledge it within 5 working days of receipt.
- Normally deal with it fully and provide a final response, in writing, within 20 working days of receipt.
- Keep you informed by letter, telephone or e-mail, as you prefer, if we need more time.
- Provide a final response, in writing, at the latest within 40 working days of receipt.
- Liaise, at your request, with anyone acting formally on your behalf.

If you are not satisfied with our final response, or if we exceed the response timescales, you may refer the complaint to The Property Ombudsman scheme (TPOs): Tel: 01722 333306, E-mail: <u>admin@tpos.co.uk.</u>



We will co-operate fully with the Ombudsman during an investigation and comply with his final decision. Complaints should be sent to:

Martin Lucass Commercial Director GeoSmart Information Limited Suite 9-11, 1st Floor, Old Bank Buildings, Bellstone, Shrewsbury, SY1 1HU Tel: 01743 298 100 <u>martinlucass@geosmartinfo.co.uk</u>



15 Terms and conditions, CDM regulations and data limitations



Terms and conditions can be found on our website: <u>http://geosmartinfo.co.uk/terms-conditions/</u> CDM regulations can be found on our website: <u>http://geosmartinfo.co.uk/knowledge-hub/cdm-2015/</u> Data use and limitations can be found on our website: <u>http://geosmartinfo.co.uk/data-limitations/</u>